

# ESTIMATION OF DIFFUSIONAL THERMOEFFECT CONTRIBUTION TO HEAT TRANSFER IN GAS MIXTURES IN ELECTRIC FIELD (STEADY STATE)

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*(Received 25 December 1974)*

**Abstract**—The methods to estimate the contribution of the diffusional thermoeffect to total heat transfer in a gas mixture in the electric field are given. Consideration is made of the case of a steady state.

## NOMENCLATURE

$\alpha_T$ ,	thermodiffusional constant;
$k_T$ ,	thermodiffusional ratio;
$\lambda_0$ ,	thermal conductivity of a mixture with uniform concentration;
$\lambda_\infty$ ,	thermal conductivity of a mixture in steady state;
$\tilde{\lambda}_\infty$ ,	thermal conductivity of a mixture in the presence of an electric field;
$\lambda_{D^T}$ ,	diffusional thermoeffect contribution to thermal conductivity of a mixture;
$\tilde{\lambda}_{D^T}$ ,	diffusional thermoeffect contribution to thermal conductivity of a mixture in the presence of an electric field;
$D_{12}$ ,	mutual diffusion coefficient;
$P$ ,	pressure;
$T$ ,	temperature;
$x_1$ ,	concentration of a light component;
$n_1$ ,	numerical density of a light component;
$n$ ,	total numerical density;
$\bar{v}$ ,	diffusional molecular velocity of 1st component;
$\tilde{v}_1$ ,	diffusional molecular velocity of 1st component in the presence of an electric field;
$q$ ,	heat flux;
$\tilde{q}$ ,	heat flux in the presence of an electric field;
$D_1^T$ ,	thermodiffusion coefficient.

**CONTRIBUTION** of the diffusional thermoeffect to heat conduction without an electric field in steady systems with a temperature gradient is defined by [1]:

$$\lambda_{D^T} = \lambda_0 - \lambda_\infty = \frac{PD_{12}}{T} \alpha_T k_T. \quad (1)$$

By analogy with equation (1) contribution of the diffusional thermoeffect to heat transfer in gas mixtures in the presence of an electric field is defined by:

$$\tilde{\lambda}_{D^T} = \lambda_0 - \tilde{\lambda}_\infty. \quad (2)$$

If an electric field is imposed on a gas mixture, then its effect will be manifested by changes in the diffusional velocity

$$\tilde{v}_i = \frac{n^2}{n_i \rho} \sum_j m_j D_{ij} \tilde{\mathbf{d}}_i - \frac{1}{n_i m_i} D_i^T \frac{\partial \ln T}{\partial \mathbf{r}}, \quad (3)$$

where

$$\tilde{\mathbf{d}}_i = \mathbf{d}_i - \frac{n_i m_i}{P \rho} \left( \frac{\rho}{m_i} \mathbf{x}_i - \sum_j n_j \mathbf{x}_j \right), \quad (4)$$

and  $\mathbf{x}_i$  and  $\mathbf{x}_j$  are the external forces due to the electric field which influence molecules of the  $i$ th and  $j$ th species; the second term in relation (4) is the contribution of the electric field to the component concentration vector.

Re-write relation (3) in the form:

$$\tilde{v}_i = \bar{v}_i + \frac{n^2}{n_i \rho} \sum_j m_j D_{ij} \frac{n_i}{n} \left\{ \frac{n_i}{\rho} \mathbf{x}_i - \frac{n_i m_i}{P \rho} \sum_i n_i \mathbf{x}_j \right\} \\ = \bar{v}_i + \bar{v}_i^*,$$

where

$$\bar{v}_i^* = \frac{n^2}{n_i \rho} \sum_j m_j D_{ij} \frac{n_i}{n} \left\{ \frac{n_i}{P} \mathbf{x}_i - \frac{n_i m_i}{P \rho} \sum_i n_i \mathbf{x}_j \right\}. \quad (5)$$

It may be shown that the heat flux density vector in the presence of an electric field is defined by:

$$\tilde{\mathbf{q}} = \mathbf{q} + \frac{1}{2} k T \sum_i n_i \bar{v}_i^* + \frac{k T}{n} \sum_{ij} \frac{n_j D_i^T}{m_i D_{ij}} (\bar{v}_i^* - \bar{v}_j^*), \quad (6)$$

where

$$\mathbf{q} = -\lambda_0 \frac{\partial T}{\partial \mathbf{r}} + \frac{1}{2} k T \sum_i n_i \bar{v}_i + \frac{k T}{n} \sum_{ij} \frac{n_j D_i^T}{m_i D_{ij}} (\bar{v}_i - \bar{v}_j)$$

is the heat flux density vector with no electric field. For a binary gas mixture of polar (subscript 1) and non-polar (subscript 2) molecules,  $\mathbf{x}_1 = \text{grad } \mu E$ ,  $\mathbf{x}_2 = 0^*$  where  $\mu$  is the dipole moment,  $E$  is the electric field strength, the expression for the vector of the heat flux density in the coordinate system moving with a mean numerical velocity takes the form:

$$\tilde{\mathbf{q}} = \mathbf{q} + \frac{x_2^2 x_1 k_T m_1 m_2^2 P D_{12}}{k T (m_1 x_1 + m_2 x_2)^3} \mathbf{x}_1 \quad (7)$$

Since the mass flow in a steady state is zero, then

$$\tilde{\mathcal{T}}_1 = n_1 m_1 \tilde{v}_1 = \frac{n^2}{\rho} m_1 m_2 D_{12} \tilde{\mathbf{d}}_1 - D_1^T \frac{\partial \ln T}{\partial \mathbf{r}} = 0.$$

\*Experiments on thermal conductivity of mixtures in an electric field are carried out just for the case considered [2-3].

Hence

$$-\frac{n^2}{\rho} m_1 m_2 D_{12} \frac{n_1 kT}{P x_1} \frac{\partial x_1}{\partial \mathbf{r}} - \frac{n^2}{\rho} \frac{m_1 m_2 D_{12} n_1}{P} \mathbf{x}_1 - D_1^T \frac{1}{T} \frac{\partial T}{\partial \mathbf{r}} = 0$$

and

$$\mathbf{x}_1 = - \left( \frac{kT}{x_1} \frac{dx_1}{dT} + \frac{P k_T}{n_1 T} \right) \frac{\partial T}{\partial \mathbf{r}}. \quad (8)$$

With regard for expression (8) relation (7) assumes the form

$$\begin{aligned} \tilde{\mathbf{q}} &= \mathbf{q} - \frac{PD_{12} x_2^2 m_1 m_2 k_T^2}{(m_1 x_1 + m_2 x_2)^3} \left[ \frac{1}{k_T} \frac{dx_1}{dT} + \frac{1}{T} \right] \frac{\partial T}{\partial \mathbf{r}} \\ &= - \left[ \lambda_0 - \lambda_{D^T} + \frac{PD_{12} x_2^3 m_1 m_2^2 k_T^2}{(m_1 x_1 + m_2 x_2)^3} \left( \frac{1}{k_T} \frac{dx_1}{dT} + \frac{1}{T} \right) \right] \frac{\partial T}{\partial \mathbf{r}} \\ &= - \lambda_\infty \frac{\partial T}{\partial \mathbf{r}}. \end{aligned} \quad (9)$$

It may be shown that

$$\tilde{\lambda}_{D^T} = \lambda_0 - \tilde{\lambda}_\infty = \lambda_{D^T} \left[ 1 + C_1 C_2^3 \left( 1 + \frac{T}{k_T} \frac{dx_1}{dT} \right) \right]. \quad (10)$$

where  $C_i = (x_i m_i)/(x_i m_i + x_j m_j)$  is the mass concentration of the  $i$ th species.

With no electric field,

$$\frac{dx_1}{dT} = - \frac{k_T}{T} \quad \text{and} \quad \tilde{\lambda}_{D^T} = \lambda_{D^T}.$$

Since  $3kT = \mu E$ , then

$$\mathbf{x}_1 = \operatorname{grad} \mu E = 3k \operatorname{grad} T. \quad (11)$$

With the aid of expressions (8) and (11) we have:

$$\frac{dx_1}{dT} = - \frac{x_1}{T} (3 - k_T) \quad (12)$$

and the contribution of the diffusional thermoeffect to heat transfer in gas mixtures in an electric field (steady state) is estimated by:

$$\tilde{\lambda}_{D^T} = \lambda_{D^T} \left[ 1 - C_1 C_2^3 \left\{ 1 - \frac{x_1}{k_T} (3 - k_T) \right\} \right]. \quad (13)$$

#### REFERENCES

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### ESTIMATION DE LA CONTRIBUTION DE L'EFFET THERMODIFFUSIONNEL AU TRANSFERT DE CHALEUR EN MELANGE GAZEUX DANS UN CHAMP ELECTRIQUE (ETAT STATIONNAIRE)

**Résumé**—Les méthodes pour estimer la contribution de l'effet thermo-diffusionnel au transfert de chaleur global, sont données pour un mélange de gaz dans un champ électrique. On considère le cas de l'état stationnaire.

### ABSCHÄTZUNG DES BEITRAGES DES DIFFUSIONALEN THERMOEFFEKTES ZUM WÄRMETRANSPORT IN GASMISCHUNGEN IM ELEKTRISCHEN FELD

**Zusammenfassung**—Die Methoden zur Abschätzung des Beitrags des diffusionalen Thermoeffekts zum gesamten Wärmetransport in einer Gasmischung im elektrischen Feld werden angegeben. Die Betrachtungen gehen vom Fall eines stabilen Zustandes aus.

### ОЦЕНКА ВКЛАДА ДИФФУЗИОННОГО ТЕРМОЭФФЕКТА В ПЕРЕНОС ТЕПЛА В ГАЗОВЫХ СМЕСЯХ, НАХОДЯЩИХСЯ В ЭЛЕКТРИЧЕСКОМ ПОЛЕ (СТАЦИОНАРНОЕ СОСТОЯНИЕ)

**Аннотация**—В статье приводится методика оценки вклада диффузионного термоэффекта в суммарный перенос тепла в газовой смеси, находящейся в электрическом поле. Рассмотрен случай стационарного состояния.